Cementitious Barrier Partnership (CBP) Toolsets

Kevin G. Brown

Vanderbilt University and CRESP Cementitious Barriers Partnership

Performance & Risk Assessment Community of Practice
Technical Exchange Meeting
December 11-12, 2014
Las Vegas NM



































Project Team Members

Vanderbilt University & CRESP

D. Kosson*, K.G. Brown*, S. Mahadevan, J. Branch, F. Sanchez

Savannah River National Laboratory (SRNL)

C. Langton*, G. Flach*, H. Burns*, R. Seitz, S. Marra

Energy Research Centre of The Netherlands (ECN) & CRESP

H. van der Sloot (HvdS Consultancy), J.C.L. Meeussen (NRG), P. Seignette

National Institute of Standards and Technology (NIST)

K. Snyder, J. Bullard, P. Stutzman

Nuclear Regulatory Commission (NRC)

D. Esh, M. Furman, J. Phillip

*Project Leadership Team

SIMCO Technologies, Inc. (Canada)

E. Samson, J. Marchand

DOE-EM Project Manager: Pramod Mallick

















Key Questions

- Waste Forms and Disposal Systems
 - What is the rate of release for hazardous contaminants and radionuclides. under a range of scenarios?
 - What is the evolution of system pH and impact on hazardous contaminant and radionuclide release?
 - What is the evolution of pore structure and impact on release and transport?
 - What are the effects of cracking on release and transport? How do we characterize the initial "cracked state"?
 - What is the rate and impact of aging processes (oxidation (Tc-99), carbonation, leaching) on performance?
- Structural Systems Performance
 - What is the remaining service life of the structure?
 - What are the impacts of ingress of aggressive species (chloride, sulfate, CO_2 , O_2) on structural performance and service life prediction?
- → CBP Software ToolBox Version 2.0 Release (January 2014)



















Primary Near-term Applications

Hanford Site

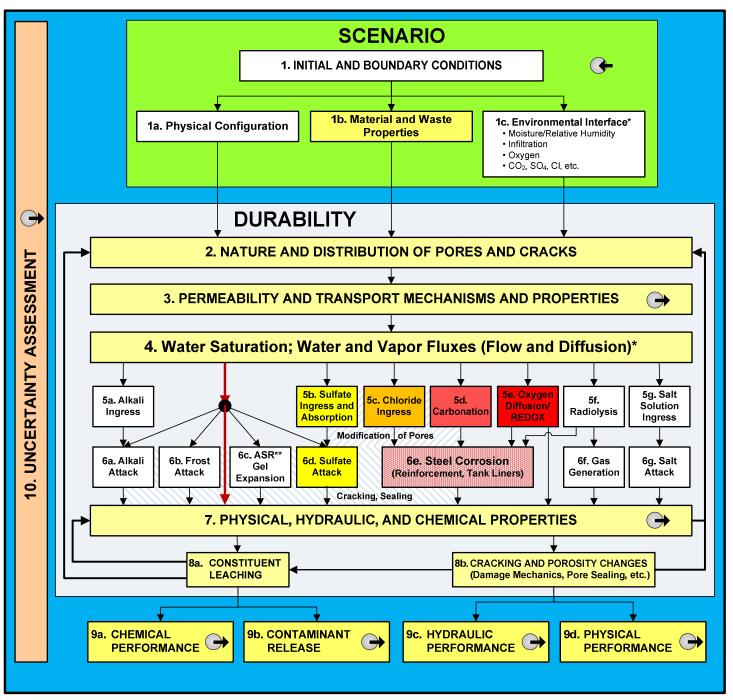
- HLW single shell tank integrity
- Waste Management Areas C/A/AX HLW tank closure assessment
- Integrated Disposal Facility performance assessment
- Source term characterization for Cast Stone (secondary waste, LAW supplemental treatment)
- In-situ grouting performance

Savannah River Site

- Saltstone performance assessment including special analyses
- Disposal vaults and other concrete facilities

Nuclear Energy

- Dry cask storage performance
- License extension



Specifications, Properties, and Phenomena for the Evaluation of Performance of Cementitious Barriers

Key Processes

Current

Chloride attack
Sulfate attack
Carbonation
Decalcification
Leaching

In-development

Cracking
Oxidation
Properties
estimation
Variable saturation
Alkali-silica reaction

















CBP Software Toolbox—Available Scenarios

STADIUM® scenarios **Waste material Concrete barrier** Soil (e.g., Saltstone or (e.g., Vault) **Cast Stone**) Waste material **Concrete barrier** (e.g., Saltstone or (e.g., Vault) **Cast Stone**) LeachXS™/ORCHESTRA scenarios **Concrete barrier** SO₄² (e.g., Vault) CO₂(g) Concrete Steel liner tank wall O₂(g) **Cracked Grout with** Percolating **Radial Diffusion** Waste layer Water (Post-closure)

Multi-layered sulfate ingress or chloride attack case

Simplified two-layer sulfate ingress or chloride attack case

Simplified one-layer sulfate attack case with boundary condition representing salt waste

Simplified one-layer carbonation case ignoring steel liner with boundary condition representing gas ingress of CO₂ and O₂

Simplified one-layer percolation with radial diffusion case ignoring waste layer with boundary condition representing percolating water



Example Applications of the CBP Toolbox

Savannah River Site

- Saltstone sulfate attack, leaching, and uncertainty analysis
- Saltstone characterization and sulfate ingress/reaction
- FY13 Saltstone Special Analysis

Hanford Site

 Low temperature waste form (Cast Stone) development and modeling for Secondary Waste and LAW Treatment

Representative HLW Tank

- Carbonation and leaching for a HLW tank closure scenario
- Probabilistic analysis of flow and leaching through a cracked HLW tank closure grout
- Combined probabilistic analysis of dome carbonation/leaching and then flow/leaching through cracked grout

CBP Software Toolbox Versions 1.0 & 2.0











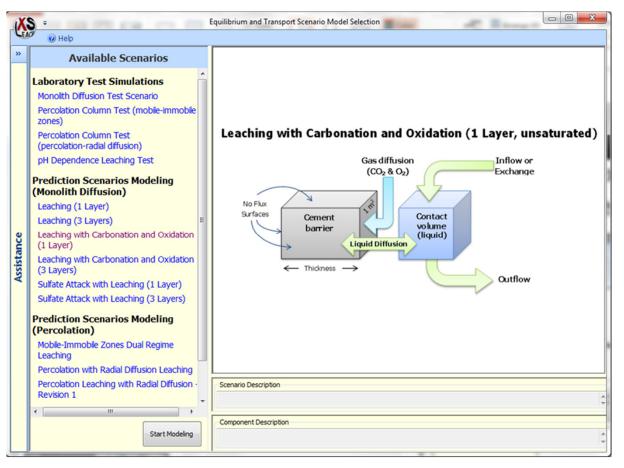








Multiple, Flexible Base Models Available in LeachXS/ORCHESTRA



- Select general field or laboratory scenario to model
- Select from existing CBP reference materials or customize materials
- Select interface conditions (e.g., fixed volume, continuous flow or intermittent flow/ exchange & solutions (e.g., "Hanford infiltration" or "saltstone pore water")
- Resulting model transferable to GoldSIM simulations









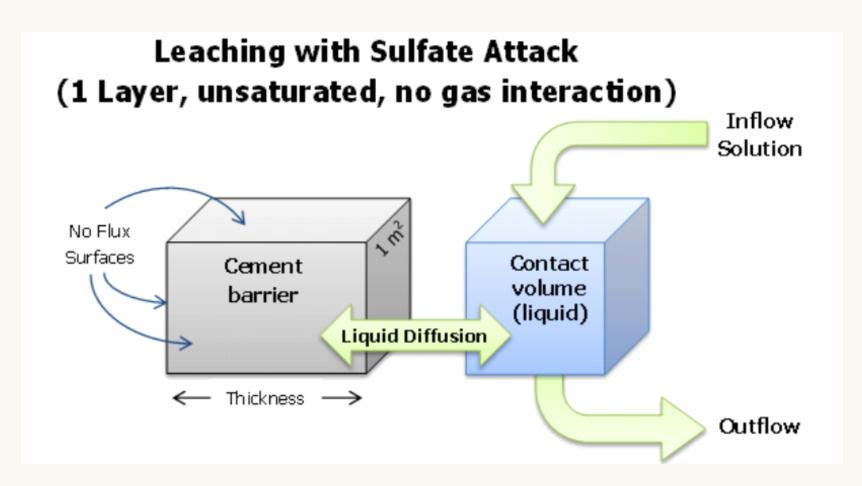








LXO Prediction Scenario – **Leaching with Sulfate Attack**











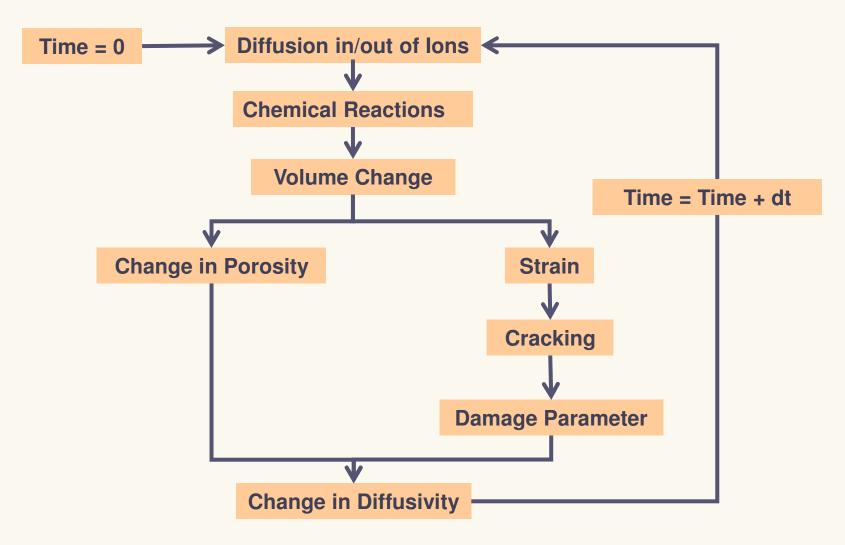








Numerical Modeling Framework















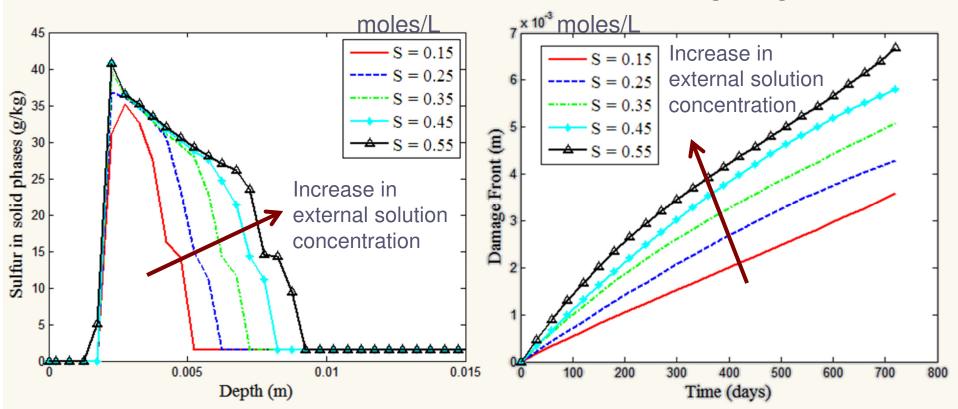




Sensitivity – External Solution Concentration



Rate of Damage Progression



Rate of damage progression increases with increase in external sulfate solution concentration

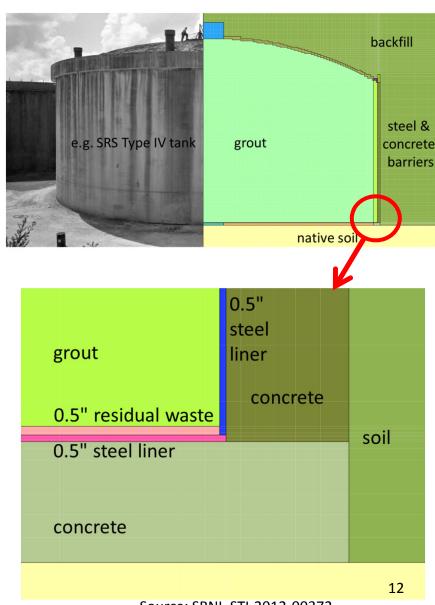


Motivation: Stabilize Residual High-Level Waste

200+ High-level waste (HLW) tanks require waste removal and closure:

- Tanks in service
 - Capacity up to ca. 4 million liters
 - Carbon steel liner within a reinforced concrete shell
- Tank closure
 - HLW retrieved to extent practical and filled with grout
 - Grout cement mixed with supplementary materials
 - Grout intended to provide structural stability and to retain residual radionuclides

Challenge – predict timeframe and radionuclide rate of release



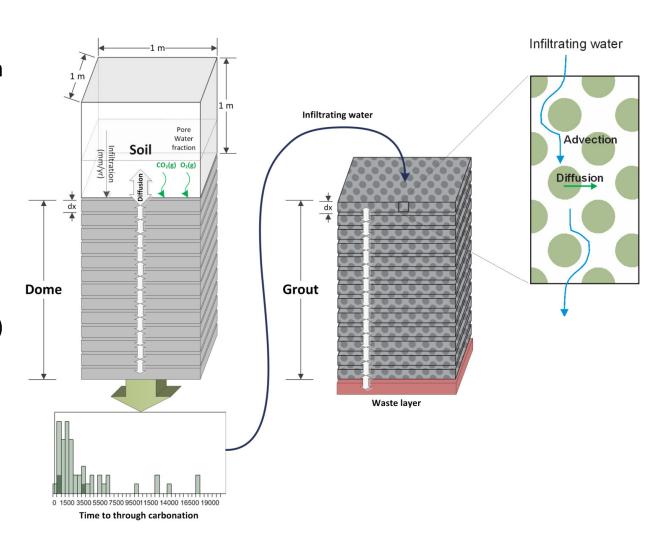
Source: SRNL-STI-2012-00372



Modeling Approach

Decouple carbonation of the dome from transport in the grout (dual regime reactive transport) model

- Carbonation of dome is a very slow process (e.g., << 1mm/yr)
- Transport in the grout
 assumed negligible until
 dome is carbonated and
 cracked (allowing infiltration)
- Stochastically model dome carbonation to generate distribution of times until cracked
- Time distribution then used to delay impact on cracked grout pH using dual regime model





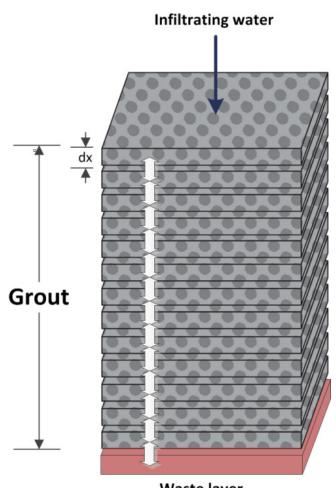
Probabilistic Grout Analysis

Non-Stochastic Parameters

- Grout thickness 10.5 m (SRS Type IV Tank)
 - Varies between 9 and 16 m (Sites, et al. 2006)

Stochastic Parameters

- Crack spacing U(1,2) m
 - Sarkar, et al. (2013)
- Infiltration Rate N(0.18, 0.051) m/yr
 - Distribution of 1,000-yr rates (WSRC-STI-2007-00184)
- Total porosity: $\phi_t U(0.20, 0.30)$
 - Sarkar, et al. (2013)
- Immobile zone porosity: ϕ_{im} N(0.221, 0.013)
 - Information from WSRC-STI-2006-00198
- Mobile volume fraction: U(0.10,0.20)
 - Sarkar, et al. (2013)
- Solid composition: N(mean, ±10%)
 - Sensitivity evaluation

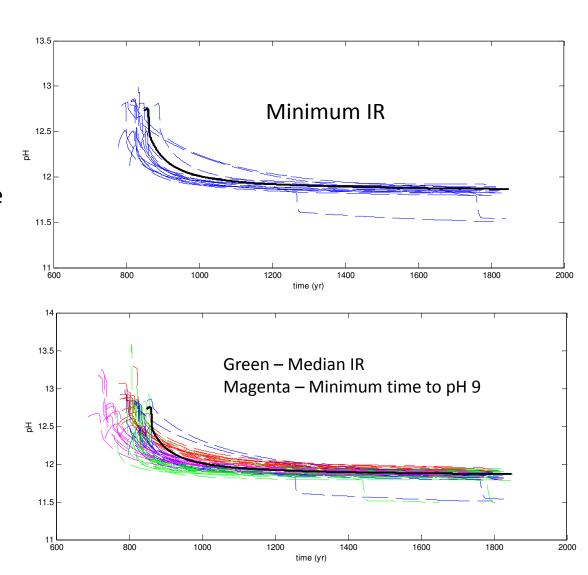


Waste layer



Coupled Analysis Results

- Simulated pH response at grout – waste layer interface
- Upper graph (blue) indicates sensitive pH response at minimum infiltration rate
- Lower graph indicates sensitive pH response depending on infiltration rate
 - Similar sensitive response found at median (green) infiltration rate
 - Waste layer not impacted until after 700 years (and likely much longer)
- Significant pH effects over the first two millenia tend to be observed as the infiltration rate is lower
 - Longer simulations may be required to better evaluate assumptions and results





FY13 Saltstone Special Analysis

CBP Software Toolbox Version 1.0





Degradation Of Cementitious Materials Associated with Saltstone Disposal Units

G. P. Flach F. G. Smith, III

November 2013 SRNL-STI-2013-00118, Rev. 1





Material Properties and Conditions

Table 9 - Initial solid phases in the concrete mixtures

Duonautias	Concretes		
Properties	Vault 1/4	Vault 2	
Hydration (%)			
Cement	80	75	
Slag	75	65	

Saltstone Disposal Unit Concrete

Fly Ash

Table 11 - Chemical analyses of pore fluids extracted after 28 days of curing

Silica Fum

Mineral phases (g.

C-S-H

Portlandite Monosulfo

(AFm) C₄FH₁₃ Species OH^{-} Na^{+} K^{+} SO_{4}^{2} Ca^{2}

(mmol/L)	
244.4	113.9
72.0	26.5

Vault 2

Vault 1/4

Table 13 - Diffusion properties estimated from migration test analyses

	Vault 2
4.29	2.80
3.69	0.41
1.65	1.08
1.42	0.16
0.0081	0.0053
0.0070	0.0008
	3.69 1.65 1.42 0.0081





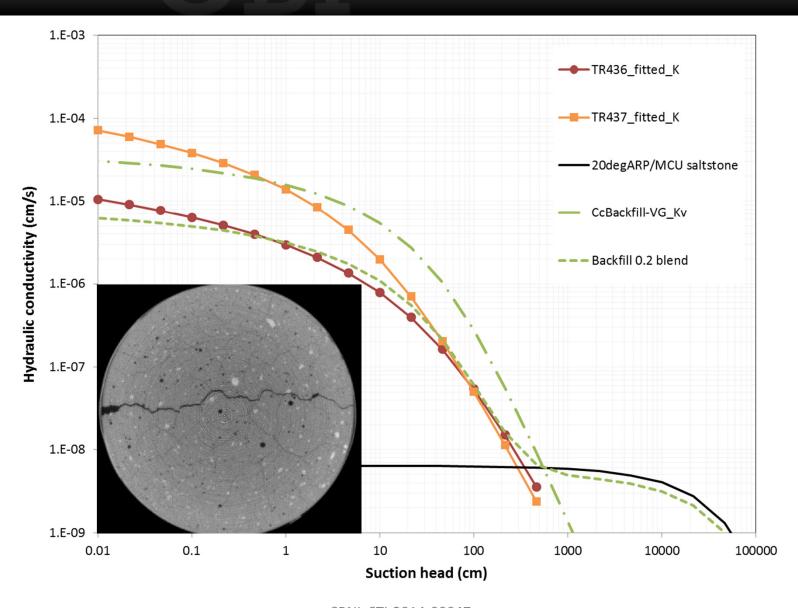
Multi-Step Outflow Extraction



Dixon, K. L. and R. L. Nichols, *Method Development for Determining the Hydraulic Conductivity of Fractured Porous Media*, SRNL-STI-2013-00522, September 2013

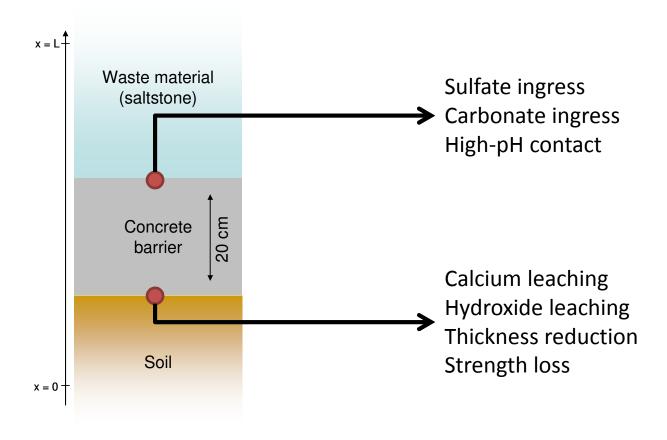


Conceptual Model Validation





Two critical interfaces:

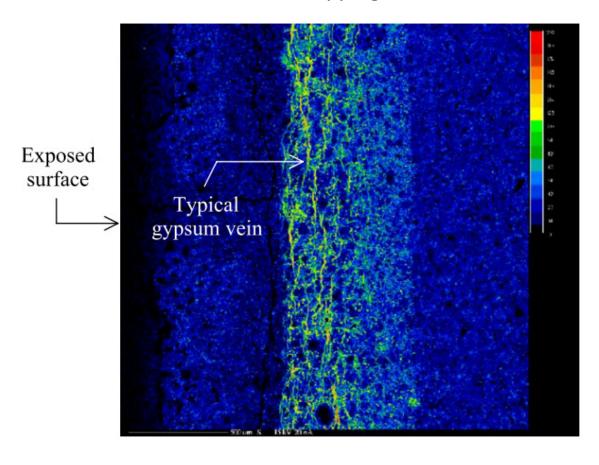




Previous work on sulfate attack

Sulfate exposure

Sulfur content mapping – 3 months

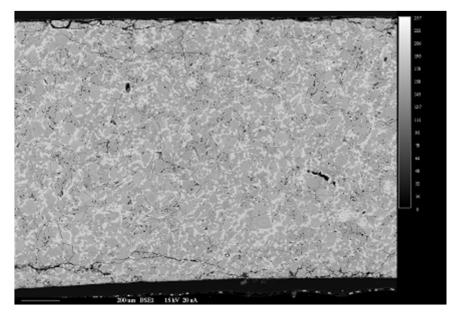




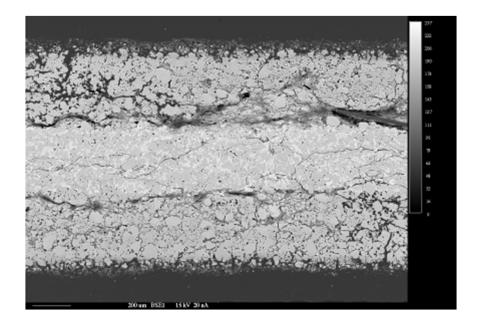
Previous work on calcium leaching

C3S paste exposed to pure water

Sound C₃S paste



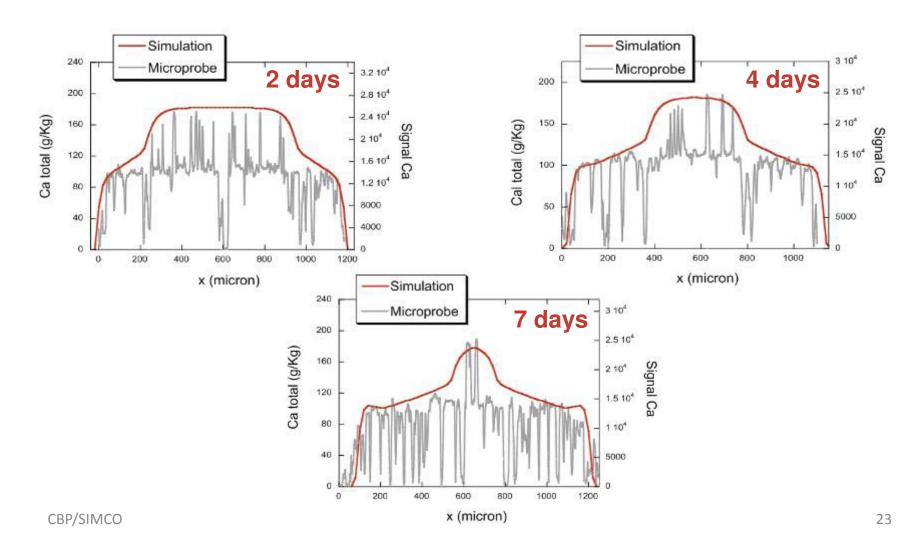
Leached C₃S paste





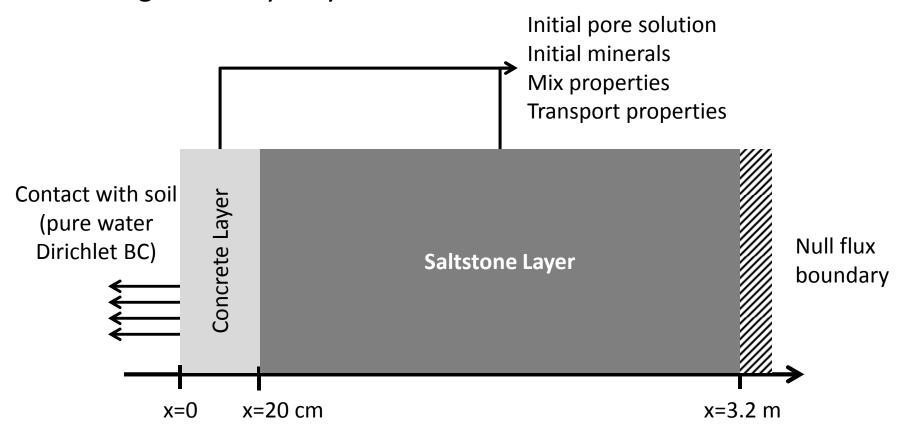
Previous work on calcium leaching

C3S paste exposed to pure water – Ca profiles





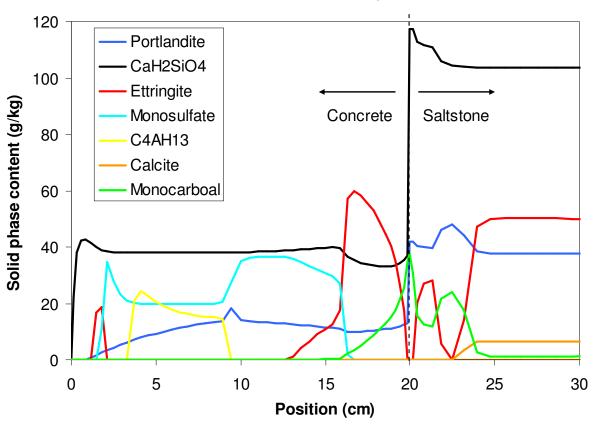
Modeling a two-layer system:





Concrete in contact with saltstone

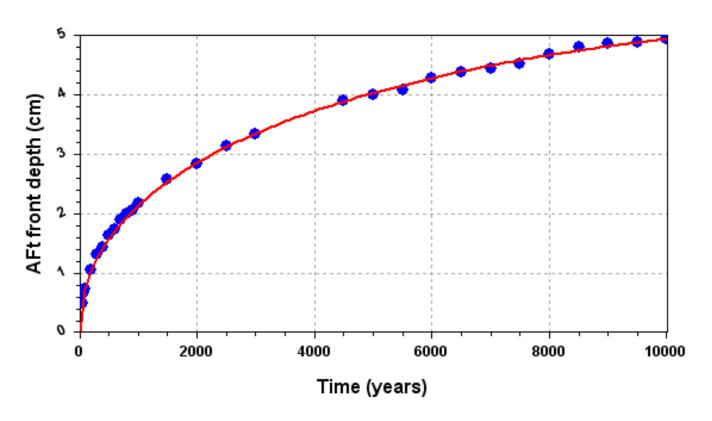
Minerals after 5000 years





Concrete in contact with saltstone

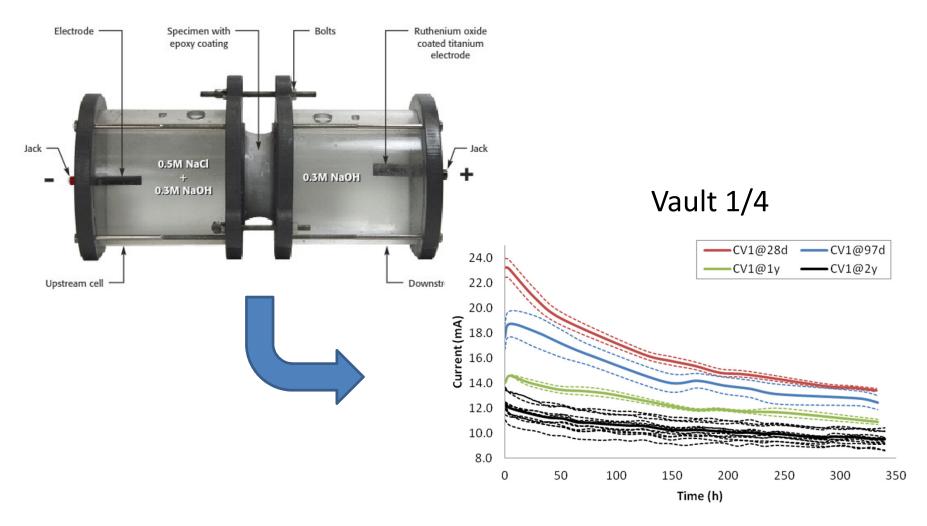
Position of the ettringite front





Concrete characterization

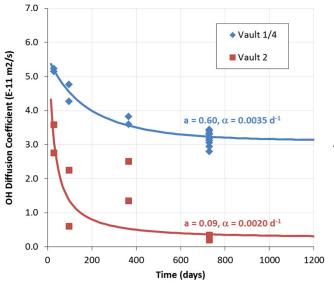
Diffusion coefficient measurements (migration test)





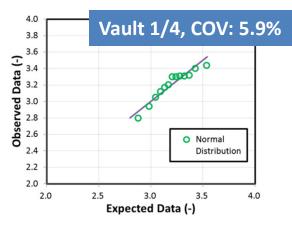
Concrete characterization

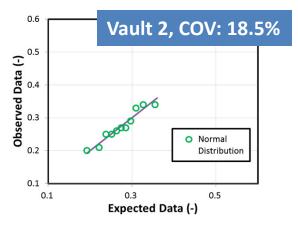
Diffusion coefficient measurements (migration test)



Avg. τ @ 2 yrs: 0.0061

Avg. τ @ 2 yrs: 0.0005





Carbonation of Microconcretes

Microconcrete sample types:

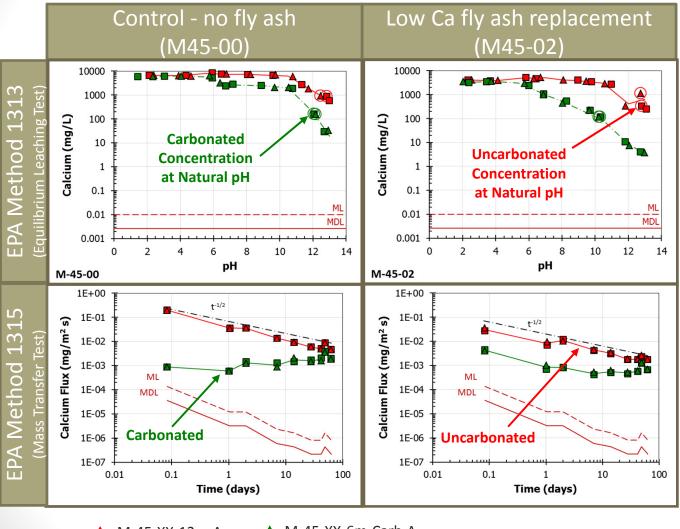
- Microconcrete with no fly ash (Control)
- Microconcretes with 45% fly ash replacement using either FA02 (bituminous coal, low calcium fly ash, ~4 wt% Ca) or FA39 (sub-bituminous coal, high calcium fly ash, ~23 wt% Ca)

Sample preparation:

- 6-month cured (100% RH)
- 6-month accelerated carbonation (5% CO₂, 65% RH)

	Control	Blend
Nominal Mix (lb/cy)	866	866
Fly ash replacement (%)	N/A	45
Composition (wt%)		
Portland Cement	22.2	12.2
Fly ash	N/A	10.0
Water	9.9	10.1
Fine Aggregate	67.9	67.7
Fly ash used (Sample code)	N/A	FA02
		FA39
Microconcrete Sample Code	M45-00	M45-02
		M45-39

Results from LEAF Methods



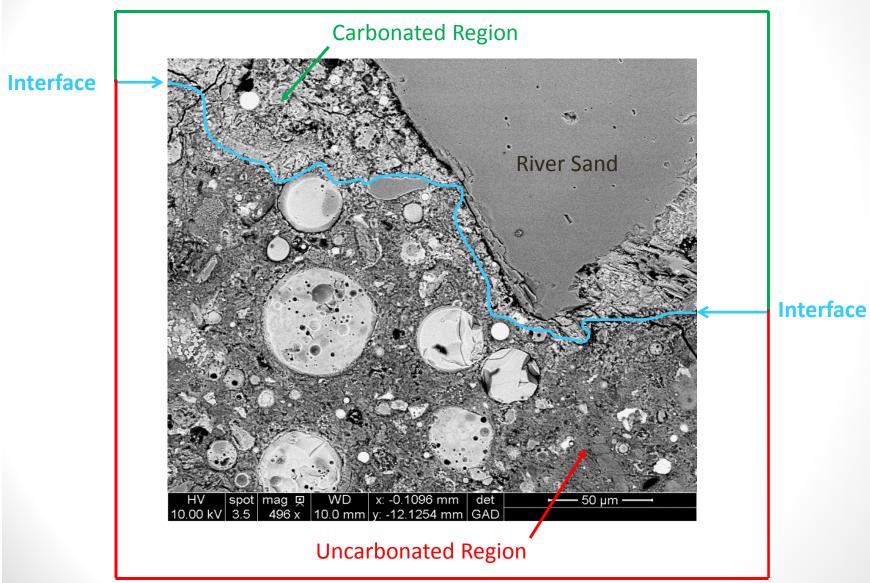
1. Solubility of Ca is lowered in carbonated materials compared to non-carbonated materials at their respective natural pH

2. Initial flux of Ca is lower for carbonated materials but approaches the non-carbonated flux as the leaching front surpasses the carbonated front

- ▲ M-45-XX-12m-A
- ▲ M-45-XX-6m-Carb-A
- M-45-XX-12m-B
- M-45-XX-6m-Carb-B
- M-45-XX-12m Mean
- M-45-XX-6m-Carb Mean

21

Carbonation Microstructure



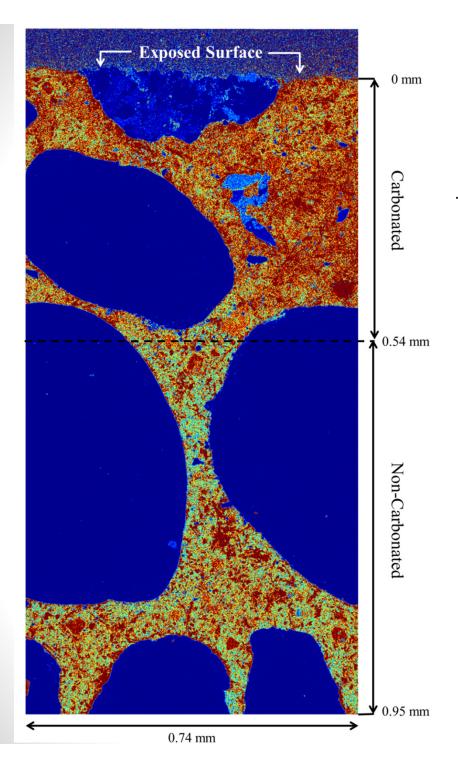
*Ex: M45-02 (low Ca FA replacement)

PA COF Jeciliii

Carbonation Profile

The material is not homogeneous

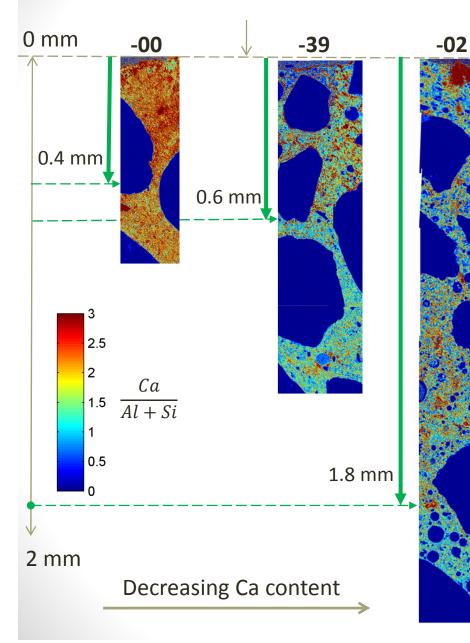
- Different layers / preferential pathways for the carbonation
- Large blue areas are the fine aggregate and the little blue ones are the epoxy from the sample preparation
- Migration of constituents to the carbonation interface based on their solubilities
- Accumulation of calcium
- Analogous behavior for pH & redox sensitive species



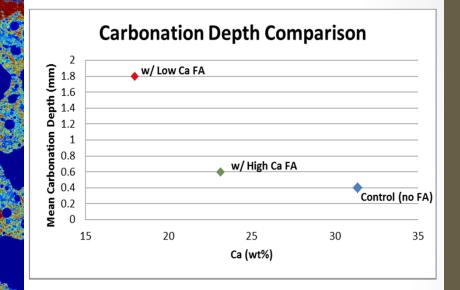
11 December 2014

PA COP Technical Exchange Meeting

SEM-EDS Carbonation Profile



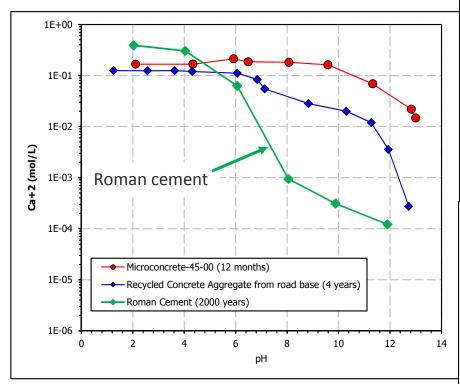
Exposed Surface



Туре	Mean Depth (mm)
Control	0.4
w/ High Ca FA	0.6
w/ Low Ca FA	1.8

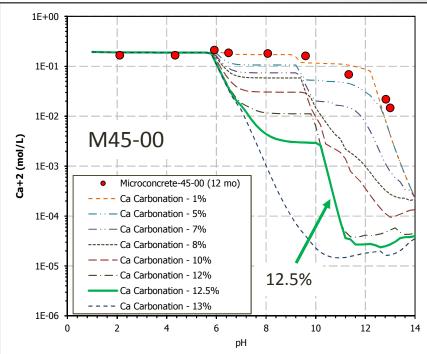
- Ca wt% is of the unhydrated Portland cement and fly ash (excluding fine aggregates)
- Ca wt% estimated by Method 3052B, test does not include C

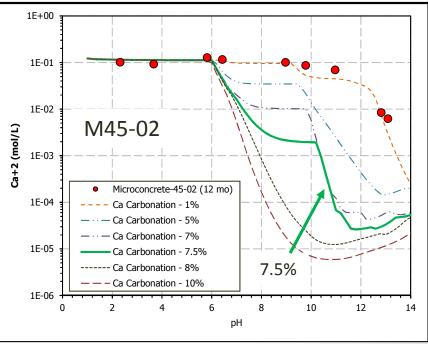
Carbonation of Cement Materials



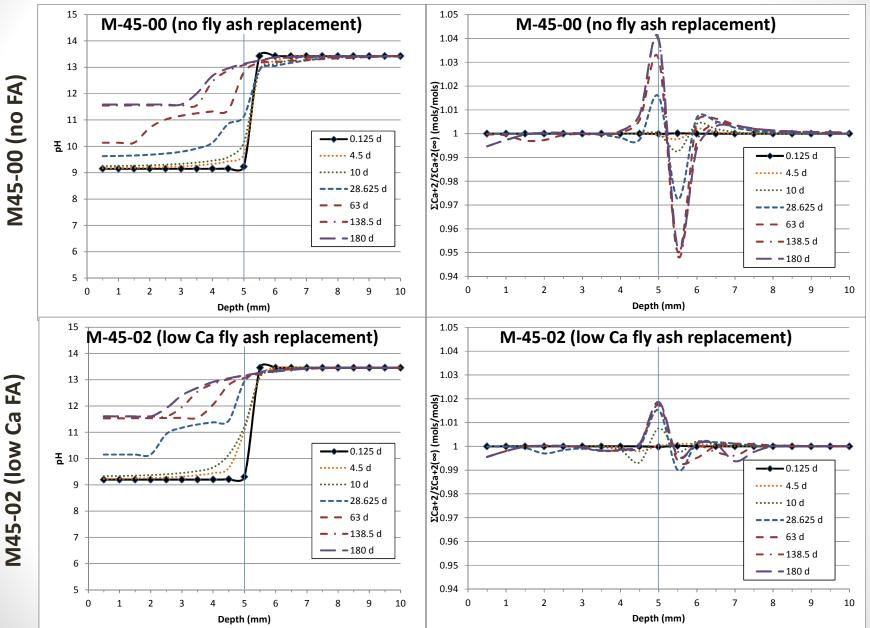
Degree of Carbonation

- Modeled by input CO₃ content
- 2000-yr-old Roman Cement (green diamonds) – completely carbonated





Monolith Diffusion Results













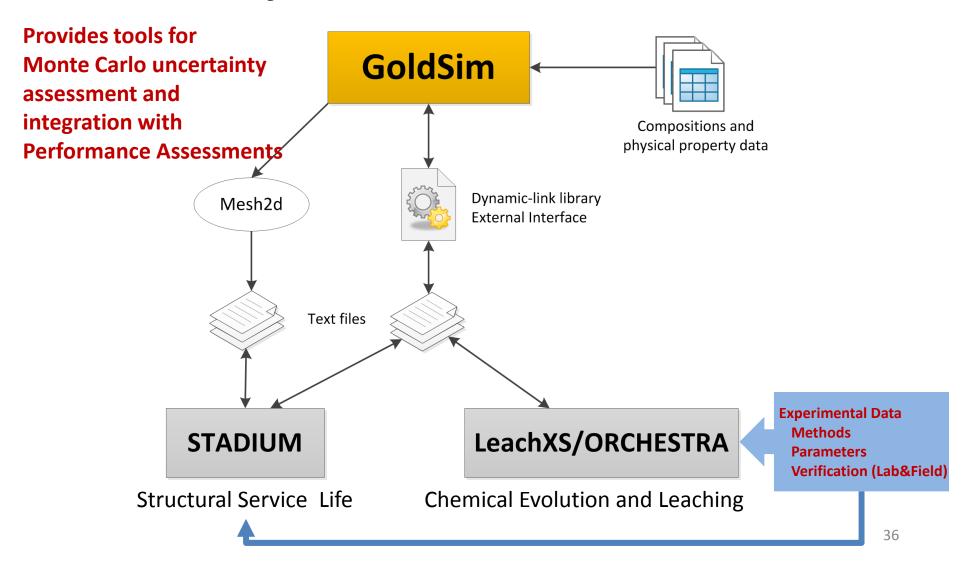








Summary of the CBP Software ToolBox





SRS PA Support Summary

- CBP software data and tools can engage the PA process in multiple ways
 - Provide higher fidelity models for particular phenomena
 - Support model abstraction
 - CBP tools are 'GoldSim-ready'
 - Material characterization
- CBP data and software have proven to be useful in the Savannah River Site Saltstone PA
 - Cementitious material degradation
 - Material characterization
 - Conceptual model validation